



# *CPillar*

Crown Pillar Stability Analysis

**Verification Manual**

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## CPillar Rigid Analysis Verification

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This document presents several examples, which have been used as verification problems for *CPillar*. *CPillar* is an engineering analysis program for assessing the stability of surface or underground crown pillars, and laminated roof beds, produced by Rocscience Inc. of Toronto, Canada.

The results produced by *CPillar* agree very well with the documented examples and confirm the reliability of *CPillar* results.

# 1. CPillar Verification Problem #1

[CPillar Build 5.001]

## 1.1. Problem Description

In this verification example, the Rigid analysis results of a rectangular pillar in *CPillar* are verified against the sensitivity analysis conducted in the paper, “A Limit Equilibrium Analysis of Surface Crown Pillar Stability”, by Hoek (1989). The Rigid analysis method in *CPillar* uses the same equations as Hoek (1989), whereby only shear failure (sliding) along the abutments are considered. The computations should yield identical results.

## 1.2. Analytical Solution

The model geometry, lateral stress and strength parameters are from Hoek (1989).

### Geometry and Material Properties

Table 1-1: Pillar Geometry and Materials

Geometry Input Data	
Pillar Length (m)	7
Pillar Width (m)	20
Pillar Height (m)	5
Rock Unit Weight (MN/m <sup>3</sup> )	0.027
Overburden Unit Weight (MN/m <sup>3</sup> )	0
Water Unit Weight (MN/m <sup>3</sup> )	0.01
Pillar Permeable	Yes

### Lateral Stress

Table 1-2: Lateral Stress

Lateral Stress Input Data	
Stress Type	Gravity
Water Height (m)	5
Overburden Height (m)	0
Locked In Stress (MPa)	0
Horizontal/Vertical Kx	0.5
Horizontal/Vertical Ky	0.5

### Strength

Table 1-3: Strength Criterion

Strength Input Data	
Strength Type	Hoek-Brown
Intact UCS (MPa)	60
Rock Mass Rating <i>RMR</i>	40
Material Constant $m_i$	10
Rock Mass <i>m</i> Value*	0.1376
Rock Mass <i>s</i> Value*	$4.54 \times 10^{-5}$

\* See equations below for computation.

Rock mass  $m$  value is calculated from  $m_i$  and  $RMR$  using:

$$m = m_i \exp\left(\frac{RMR - 100}{14}\right) = (10) \exp\left(\frac{40 - 100}{14}\right) = 0.1376$$

Rock mass  $s$  value is calculated from  $RMR$  using:

$$s = \exp\left(\frac{RMR - 100}{6}\right) = 4.54 \times 10^{-5}$$

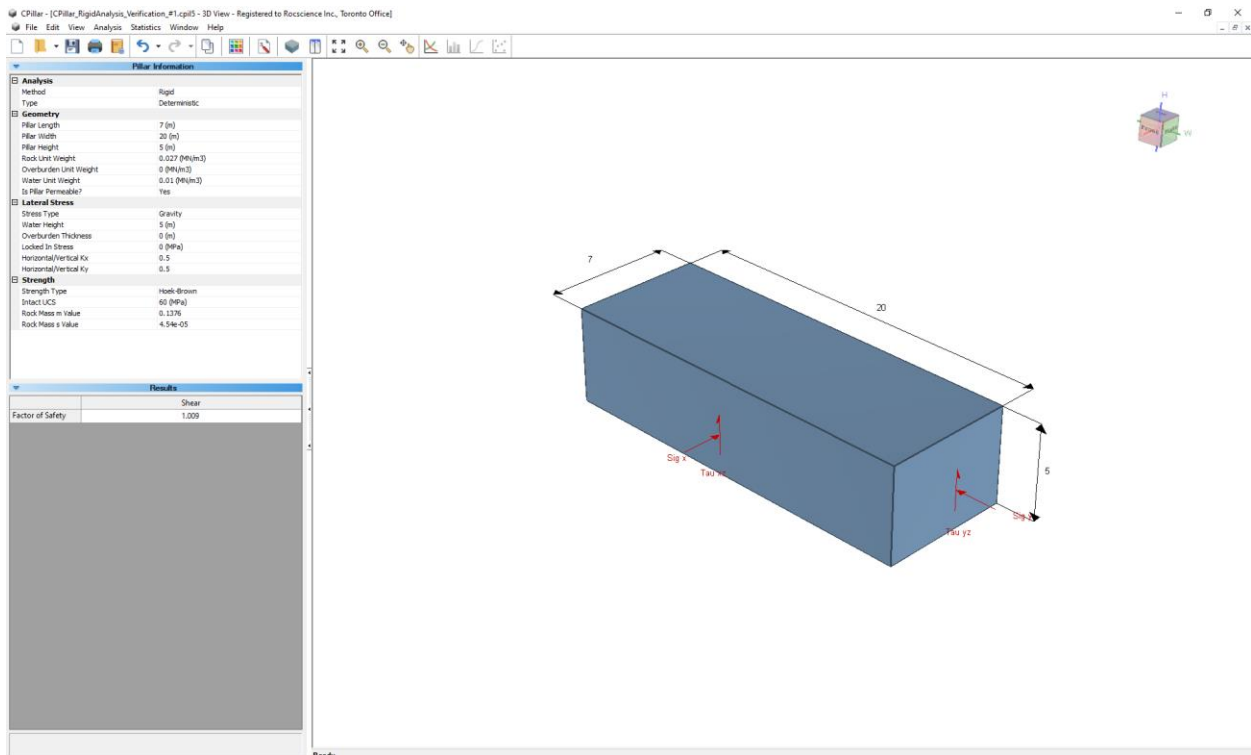
### 1.3. CPillar Analysis

#### Deterministic Analysis

Set the Analysis Method in *CPillar* to Rigid and Analysis Type to Deterministic.

Enter the input values from Table 1-1, Table 1-2, and Table 1-3 into *CPillar*.

The *CPillar* model looks like this:



#### Sensitivity Analysis

A sensitivity analysis is performed in *CPillar* to see how sensitive the Factor of Safety is to changing parameters. The following parameters were varied:

Table 1-4: Sensitivity Ranges

Sensitivity Parameter	Range	
	Minimum	Maximum
Rock Mass Rating <i>RMR</i>	1	80
Horizontal/Vertical Stress Ratio <i>K</i> ( $K_x = K_y$ )	0.1	5
Water Height $Z_w$ (m)	0	5
Pillar Height $Z$ (m) ( $Z_w = Z$ )	0.1	30
Material Constant $m_i$	5	30
Intact UCS (MPa)	20	100

Note:

When varying the Horizontal-to-Vertical Stress Ratio ( $K$ ), both  $K_x$  and  $K_y$  are changed simultaneously in *CPillar*.

When varying Pillar Height ( $Z$ ), Water Height is changed simultaneously in *CPillar* to reflect a fully wetted pillar.

When varying Rock Mass Rating (*RMR*) or Material Constant  $m_i$ , the *CPillar* inputs for  $m$  and  $s$  are calculated based on the equations in Section 1.2.

## 1.4. Results

### Deterministic Analysis

The deterministic inputs were calibrated by Hoek (1989) to give a Factor of Safety of approximately 1. The Factor of Safety computed by *CPillar* using the deterministic inputs is  $1.009 \approx 1$ .

### Sensitivity Analysis

By comparing the sensitivity results of Hoek (1989) and *CPillar*, it can be seen that they produce identical results, with the exception of the first data point in Factor of Safety vs.  $K$  plot. This discrepancy is due to the fact that *CPillar* will set a very small effective lateral stress limit (close to 0) when the water pressure exceeds the total lateral stress. This ensures that the effective lateral stress used to compute the shear strength is never less than zero.

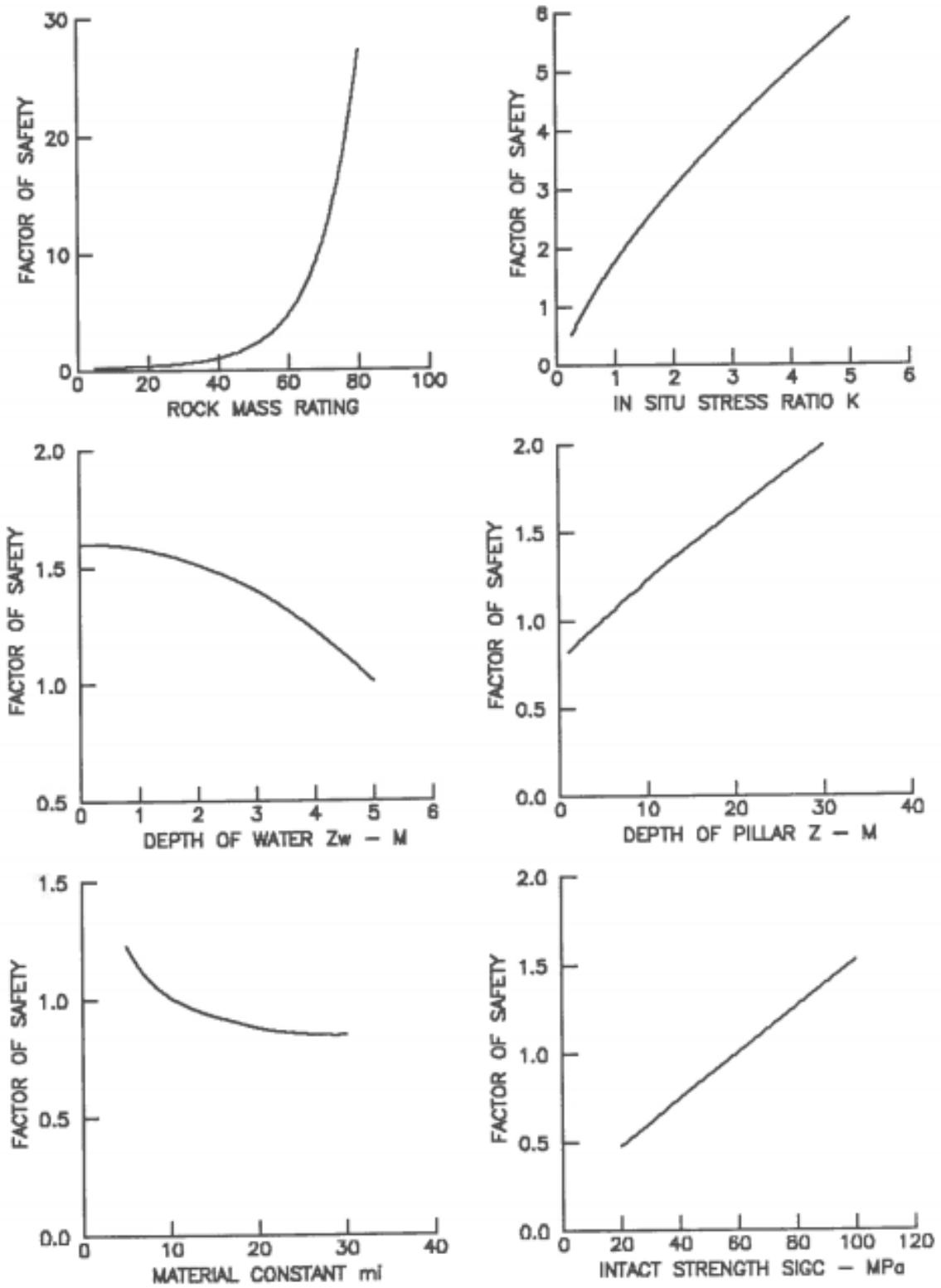
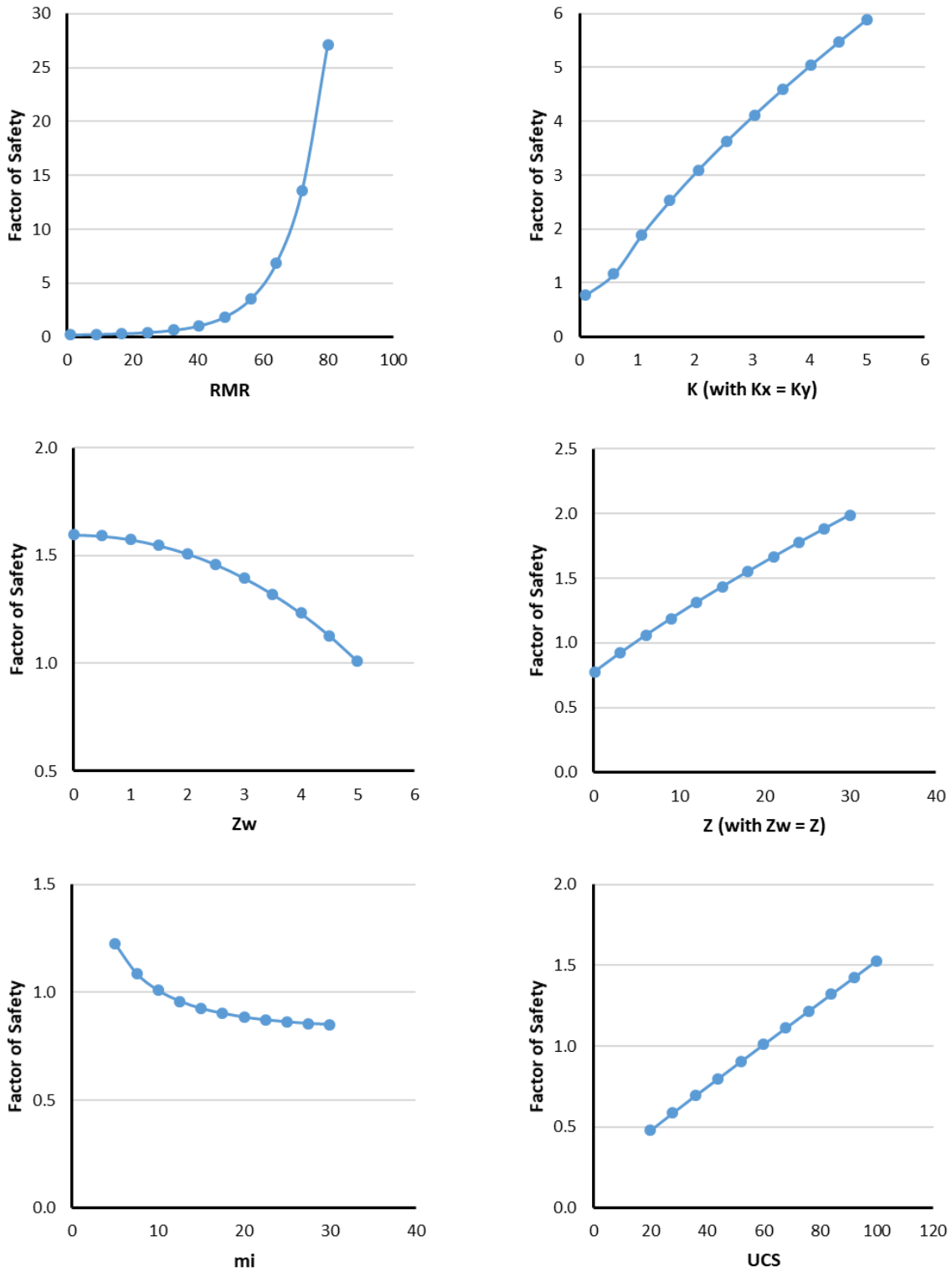


Figure 1-1: Sensitivity Plots Provided by Hoek (1989)



**Figure 1-2: CPillar Sensitivity Analysis Results**

Therefore, CPillar's results have been verified with Hoek's results.



## References

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1. Hoek, E. (1989) A Limit Equilibrium Analysis of Surface Crown Pillar Stability. Proc. Int. Conf. on Surface Crown Pillars Active & Abandoned Metal Mines Timmins, pp. 3-13.