

6- Hoek-Brown and Generalized Hoek-Brown Material Models

Hoek-Brom failure criterion is the most common failure criterion used for rock masses. Hoek and Brown (1980a, b) introduced their failure criterion in an attempt to provide input data for the analyses required for the design of underground excavations in hard rock. The criterion was derived from the results of research into the brittle failure of intact rock by Hoek (1968) and on model studies of jointed rock mass behavior by Brown (1970). The criterion starts from the properties of intact rock and then by applying reduction factors on the basis of the characteristics of joints in a rock mass is modified to suit the rock mass behavior.

The failure criterion of the Hoek Brown model in terms of principal stresses is

$$F_s = \sigma_1 - \sigma_3 - \sigma_{ci} \left(m \frac{-\sigma_1}{\sigma_{ci}} + s \right)^{0.5} = 0 \quad (6.1)$$

where σ_{ci} is the uniaxial compressive strength of the intact material, m is the reduced value of the intact rock parameter m_i , and s is a material constant that can have the maximum value of 1.0 for intact rock.

The generalized Hoek-Brown yield surface has an additional parameter a that replaces the 0.5 power term.

$$F_s = \sigma_1 - \sigma_3 - \sigma_{ci} \left(m \frac{-\sigma_1}{\sigma_{ci}} + s \right)^a = 0 \quad (6.2)$$

To find the strength of the mass rock from intact rock properties, the Geological Strength Index (GSI) was introduced by Hoek, Wood and Shah (1992), Hoek (1994) and Hoek, Kaiser and Bawden (1995).

$$m = m_i e^{\left(\frac{GSI-100}{28-14D} \right)} \quad (6.3)$$

$$s = e^{\left(\frac{GSI-100}{9-3D} \right)} \quad (6.4)$$

$$a = \frac{1}{2} + \frac{1}{6} \left(e^{-GSI/15} - e^{-20/3} \right) \quad (6.5)$$

In above D is the disturbance factor due to blast or stress relaxation that varies from 0.0 for undisturbed in situ rock mass to 1.0 for very disturbed rock mass.

In terms of stress invariants the Generalized Hoek-Brown yield surface is

$$F_s = 2 \cos \theta \sqrt{J_2} - \sigma_{ci} \left(\frac{m}{\sigma_{ci}} \left(\frac{-I_1}{3} + \sqrt{\frac{J_2}{3}} (\sin \theta - \sqrt{3} \cos \theta) \right) + s \right)^a = 0 \quad (6.6)$$

RS² and RS³ accept peak values and residual values for the all the material properties of these two models. This means that after the initial yielding the strength of the material instantly drops to a lower residual state. The Hoek-Brown and the generalized Hoek-Brown models in RS² and RS³ are elasto-brittle-plastic material model in general. In the case where the residual values are the same as peak values the behavior is elasto-perfect-plastic.

The plastic potential function has the same form as the yield surface

$$Q_s = 2 \cos \theta \sqrt{J_2} - \sigma_{ci} \left(\frac{m_\psi}{\sigma_{ci}} \left(\frac{-I_1}{3} + \sqrt{\frac{J_2}{3}} (\sin \theta - \sqrt{3} \cos \theta) \right) \right)^a = const. \quad (6.7)$$

where m_ψ is the dilation parameter. This parameter should be less than or equal to m which makes the flow rule non-associated or associated respectively.

The dialog for defining this constitutive model is shown in Figure 6.1.

Parameter	Value
Failure Criterion	Generalized Hoek Brown (GH)
Material Type	Plastic
Intact Comp. Strength (kPa)	100
Dilation Parameter	0
mb Parameter (peak)	1
mb Parameter (resid)	1
s Parameter (peak)	0.1
s Parameter (resid)	0.1
a Parameter (peak)	0.5
a Parameter (resid)	0.5

Figure 6.1. Dialog for defining Generalized Hoek-Brown model

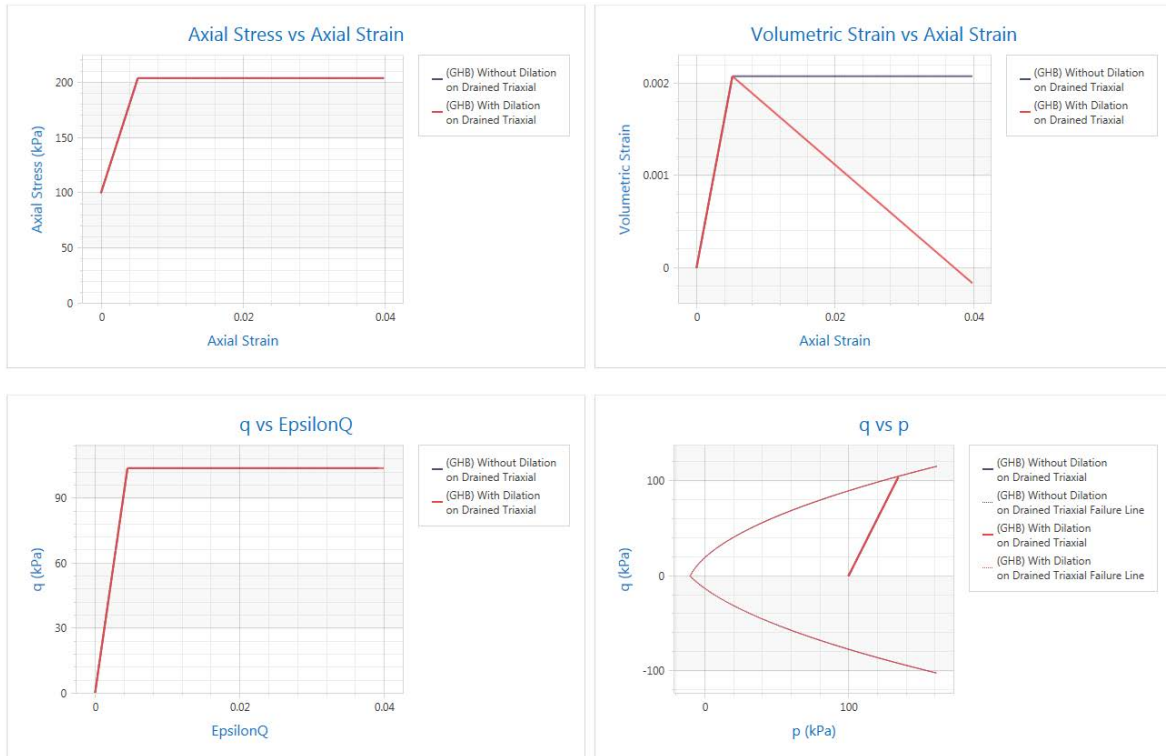


Figure 6.2. Stress paths of drained triaxial tests on materials with Generalized Hoek-Brown model

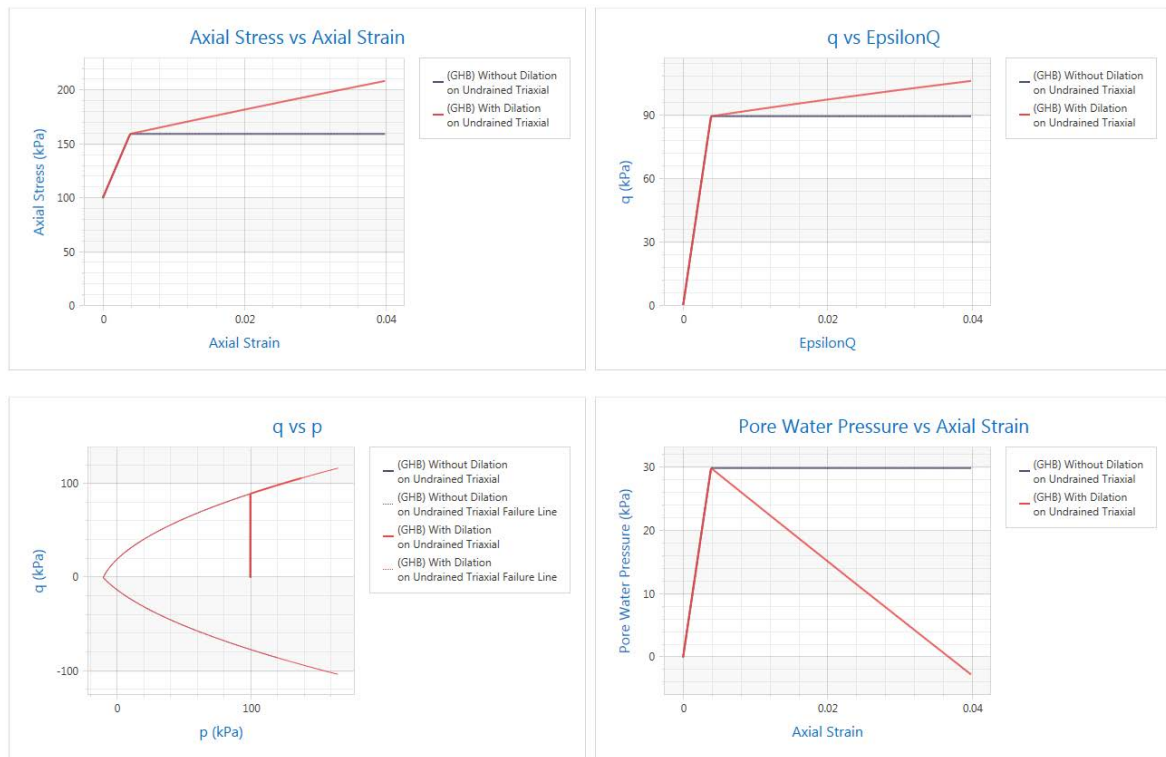


Figure 6.3. Stress paths of undrained triaxial tests on materials with Generalized Hoek-Brown model

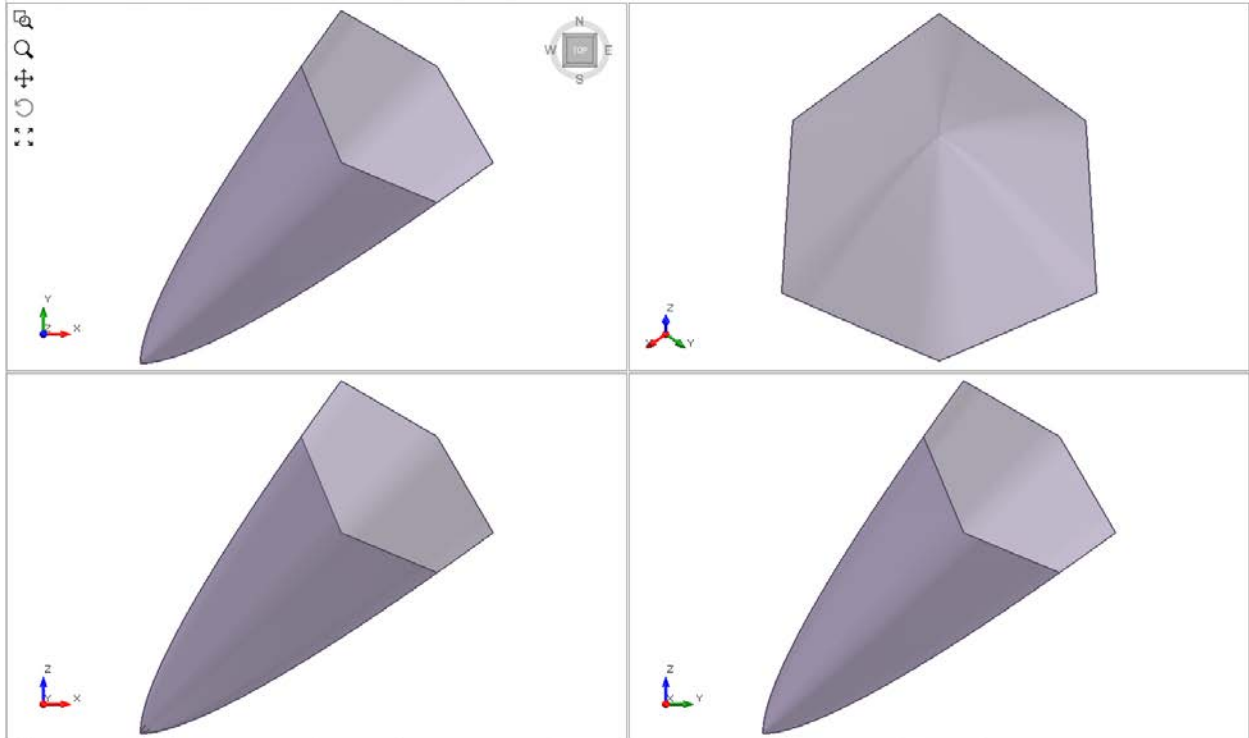


Figure 6.4. Yield surface of Generalized Hoek-Brown model in 3D stress space

Sample stress paths of drained and undrained triaxial compression tests that could be simulated with this model are presented in Figure 6.2 and 6.3. All the tests start from a hydrostatic confinement of $p = p' = 100$ kPa.

Stress paths of the drained tests include variations of axial stress and volumetric strain with increasing axial strain, variation of deviatoric stress with deviatoric strain and the stress path in p-q plane. The yield surface is also shown in the p-q plane. The simulated behavior is an elasto-perfect plastic behavior. The dilation effect is illustrated in the variation of volumetric strain with axial strain.

Stress paths of the undrained tests include the variation of axial stress and pore water pressure with increasing axial strain, variation of deviatoric stress with deviatoric strain and the stress path in p-q plane. The yield surface is also shown in the p-q plane. The dilation effect is illustrated in the plot of the stress path in p-q plane that also include the yield surface. The generation of negative pore water pressure in material with dilation leads to the increase in the effective mean stress, as the stress path lays on the yield surface and follows it to higher levels of deviatoric stress.

The yield surface of this model is a curved line in 2D stress space as shown in Figures 6.2 and 6.3 and has an irregular hexagonal pyramid shape in 3D stress space as presented in Figures 5.4. The definition of yield surface includes the Lode's angle and thus the projection of this yield surface in Π plane, with normal direction being the stress space diagonal, deviates from the circular shape of Drucker-Prager model and has a shape similar to the Mohr-Coulomb failure envelope.

The model also accept a tension cutoff. The yield surface of the tension cut off is

$$F_T = \sigma_1 - T = 0 \quad (6.8)$$

In above T is the tensile strength of the material. The flow rule for tensile failure is associated. There couple of options for the tensile strength of Hoek-Brown model. The maximum value of the tensile strength from can be calculated from the definition of the yield surface in equation 6.1 or 6.2.

$$T_{\max} = \frac{s\sigma_{ci}}{m} \quad (6.9)$$

If the tensile strength is set to a higher value than T_{\max} the program will ignore that value and use T_{\max} instead. Hoek and Martin (2014) has proposed this alternative relationship for the tensile resistance

$$T = \frac{\sigma_{ci}}{8.62 + 0.7m_i} \quad (6.10)$$

The user defined option for tensile strength is also available to the users.

References

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