

RocTopple

Topping Analysis and Support Design of Rock Slops

Verification Manual

Table of Contents

| 1. RocTop | <i>pl</i> e Block Toppling Verification | 5 |
|------------------|---|----|
| 1.1. Roc | <i>Topple</i> Verification Problem #1 | 6 |
| 1.1.1. | Problem Description | 6 |
| 1.1.2. | RocTopple Analysis | 7 |
| 1.1.3. | Building a Compatible <i>RS2</i> Model | 8 |
| 1.1.4. | UDEC Analysis | 9 |
| 1.1.5. | Results | 9 |
| 1.2. Roc | <i>Topple</i> Verification Problem #2 | |
| 1.2.1. | Problem Description | 10 |
| 1.2.2. | RocTopple Analysis | 11 |
| 1.2.3. | Building a Compatible <i>RS2</i> Model | 11 |
| 1.2.4. | UDEC Analysis | 12 |
| 1.2.5. | Results | 13 |
| 1.3. <i>Ro</i> o | Topple Verification Problem #3 | 14 |
| 1.3.1. | Problem Description | 14 |
| 1.3.2. | RocTopple Analysis | 15 |
| 1.3.3. | Building a Compatible <i>RS2</i> Model | 15 |
| 1.3.4. | UDEC Analysis | 16 |
| 1.3.5. | Results | 16 |
| 1.4. <i>Roc</i> | <i>Topple</i> Verification Problem #4 | 17 |
| 1.4.1. | Problem Description | 17 |
| 1.4.2. | RocTopple Analysis | 17 |
| 1.4.3. | Building a Compatible <i>RS2</i> Model | 17 |
| 1.4.4. | Results | |
| 1.5. Roc | <i>Topple</i> Verification Problem #5 | 19 |
| 1.5.1. | Problem Description | 19 |
| 1.5.2. | RocTopple Analysis | 19 |
| 1.5.3. | Building a Compatible <i>RS2</i> Model | |
| 1.5.4. | Results | |
| 1.6. Roc | <i>Topple</i> Verification Problem #6 | 21 |
| 1.6.1. | Problem Description | 21 |
| 1.6.2. | RocTopple Analysis | 21 |

| 1.6.3. | Building a Compatible <i>RS2</i> Model | . 22 |
|-------------------|--|------|
| 1.6.4. | Results | . 23 |
| 1.7. Roo | <i>Topple</i> Verification Problem #7 | . 24 |
| 1.7.1. | Problem Description | . 24 |
| 1.7.2. | RocTopple Analysis | . 24 |
| 1.7.3. | Building a Compatible <i>RS2</i> Model | . 25 |
| 1.7.4. | Results | . 26 |
| 1.8. <i>Ro</i> o | <i>CTopple</i> Verification Problem #8 | . 27 |
| 1.8.1. | Problem Description | . 27 |
| 1.8.2. | RocTopple Analysis | . 27 |
| 1.8.3. | Building a Compatible <i>RS2</i> Model | . 28 |
| 1.8.4. | Results | . 30 |
| 1.9. <i>Ro</i> o | <i>Topple</i> Verification Problem #9 | . 31 |
| 1.9.1. | Problem Description | . 31 |
| 1.9.2. | RocTopple Analysis | . 31 |
| 1.9.3. | Building a Compatible <i>RS2</i> Model | . 34 |
| 1.9.4. | Results | . 35 |
| 1.10. <i>Ro</i> d | <i>CTopple</i> Verification Problem #10 | . 36 |
| 1.10.1 | . Problem Description | . 36 |
| 1.10.2 | . RocTopple Analysis | . 36 |
| 1.10.3 | . Building a Compatible <i>RS2</i> Model | . 37 |
| 1.10.4 | . Results | . 37 |
| 1.11. Roo | <i>CTopple</i> Verification Problem #11 | . 38 |
| 1.11.1 | . Problem Description | . 38 |
| 1.11.2 | . RocTopple Analysis | . 38 |
| 1.11.3 | . Building a Compatible <i>RS2</i> Model | . 39 |
| 1.11.4 | . Results | .40 |
| 1.12. Roo | <i>CTopple</i> Verification Problem #12 | .41 |
| 1.12.1 | . Problem Description | .41 |
| 1.12.2 | . RocTopple Analysis | .41 |
| 1.12.3 | . Building a Compatible <i>RS2</i> Model | .42 |
| 2. RocTop | ple Block-Flexural Toppling Verification | .43 |
| 2.1. Roo | <i>Topple</i> Verification Problem #1 | .44 |
| 2.1.1. | Problem Description | .44 |

| 2.1.2. | RocTopple Analysis | 45 |
|----------|--|----|
| 2.1.3. | Building a Compatible RS2 Model | 45 |
| 2.1.4. | Results | 46 |
| 2.2. Roc | <i>Topple</i> Verification Problem #2 | 47 |
| 2.2.1. | Problem Description | 47 |
| 2.2.2. | RocTopple Analysis | 48 |
| 2.2.3. | Building a Compatible RS2 Model | 49 |
| 2.2.4. | Results | 49 |
| 2.3. Roc | <i>Topple</i> Verification Problem #3 | 50 |
| 2.3.1. | Problem Description | 50 |
| 2.3.2. | RocTopple Analysis | 51 |
| 2.3.3. | Building a Compatible RS2 Model | 51 |
| 2.3.4. | Results | 52 |
| 2.4. Roc | <i>Topple</i> Verification Problem #4 | 53 |
| 2.4.1. | Problem Description | 53 |
| 2.4.2. | RocTopple Analysis | 54 |
| 2.4.3. | Building a Compatible RS2 Model | 54 |
| 2.4.4. | Results | 55 |
| 2.5. Roc | <i>Topple</i> Verification Problem #5 | 56 |
| 2.5.1. | Problem Description | 56 |
| 2.5.2. | RocTopple Analysis | 56 |
| 2.5.3. | Building a Compatible <i>RS2</i> Model | 57 |
| 2.5.4. | Results | 58 |
| 2.6. Roc | <i>Topple</i> Verification Problem #6 | 59 |
| 2.6.1. | Problem Description | 59 |
| 2.6.2. | RocTopple Analysis | 59 |
| 2.6.3. | Results | 60 |
| 2.7. Roc | <i>Topple</i> Verification Problem #7 | 61 |
| 2.7.1. | Problem Description | 61 |
| 2.7.2. | RocTopple Analysis | 61 |
| 2.7.3. | Building a Compatible <i>RS2</i> Model | 62 |
| 2.7.4. | Results | 62 |
| | | |

1. RocTopple Block Toppling Verification

This document presents several examples, which have been used as verification problems for *RocTopple*. *RocTopple* is an engineering analysis program for performing toppling analysis and support design of rock slopes, produced by Rocscience Inc. of Toronto, Canada.

RocTopple is verified against published examples and against results produced by *RS2* and UDEC. The results produced by *RocTopple* agree very well with the documented examples and confirm the reliability of *RocTopple* results.

1.1. RocTopple Verification Problem #1

[*RocTopple* Build 2.001]

1.1.1. Problem Description

This verification looks at Example 1 in the paper:

Goodman, R. E., & Bray, J. W. (1976). Toppling of Rock Slopes. *Rock Engineering for Foundations and Slopes* (pp. 201 - 234). New York: American Society of Civil Engineers.

Four analyses of block toppling were performed in *RocTopple* and verified using *RS2* and UDEC. The analyses comprised of computing the factor of safety for examples 1a and 1b and the same examples with higher friction (page 222 of the paper), named examples 1c and 1d here. All examples include a stabilizing force on the toe of the slope. In the case of examples 1a and 1b, this force establishes limit equilibrium (FS = 1) as computed by the Goodman and Bray method.

Geometry and Material Properties

| Analysis | φ΄ (deg.) | Force on Toe Block (kN) | γ (kN/m³) |
|------------|--------------|----------------------------|--------------|
| Example 1a | 38.15 | 0.5 | 25.0 |
| Example 1b | 33.02 | 2013 | 25.0 |
| Example 1c | 38.66 | 0.5 | 25.0 |
| Example 1d | 38.66 | 2013 | 25.0 |

Table 1.1.1: Material Properties

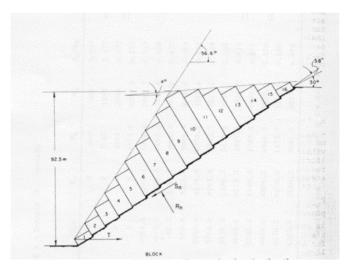


Figure 1.1.1: Geometry with 16 Blocks (Goodman and Bray, 1976)

1.1.2. RocTopple Analysis

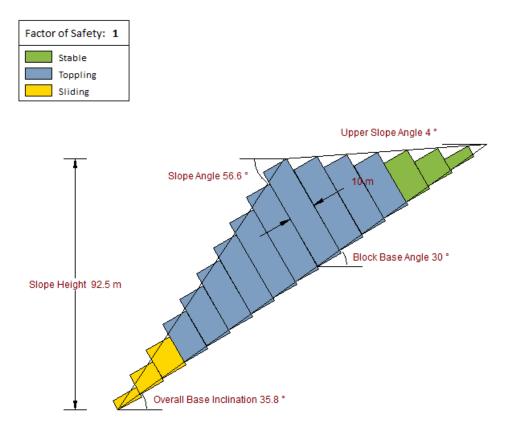


Figure 1.1.2: *RocTopple* Model using Goodman and Bray Input Geometry (16 Blocks)

1.1.3. Building a Compatible RS2 Model

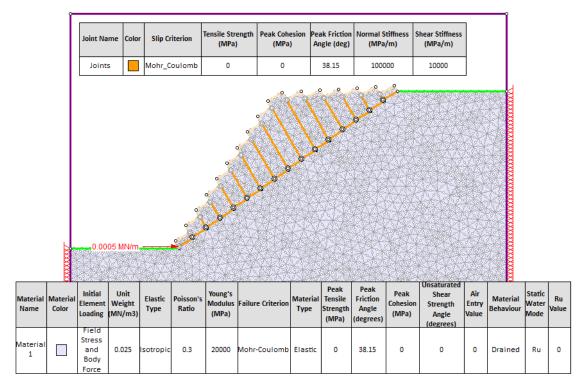


Figure 1.1.3: RS2 Model of Example 1a (Geometry Exported from RocTopple)

Critical SRF: 1.001

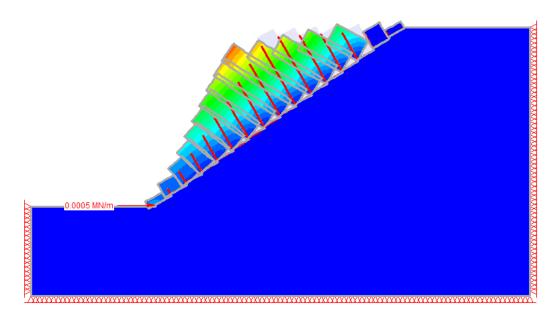


Figure 1.1.4: RS2 Results of Example 1a at Critical SRF (Total Displacement Contours)

1.1.4. UDEC Analysis

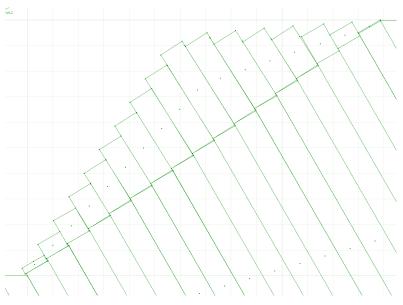


Figure 1.1.5: Deformation in UDEC

1.1.5. Results

| y |
|---|
| y |

| | RocTopple | RS2 | UDEC | Goodman and Bray |
|------------|-----------|------|------|---------------------|
| Example 1a | 1.00 | 1.00 | 0.99 | 1.0 |
| Example 1b | 1.00 | 0.98 | 1.00 | 1.0 |
| Example 1c | 1.02 | 1.01 | 1.00 | 1.02 |
| Example 1d | 1.23 | 1.21 | 1.24 | 1.23 |

1.2. RocTopple Verification Problem #2

[RocTopple Build 2.001]

1.2.1. Problem Description

This verification looks at Example 2 in the paper:

Goodman, R. E., & Bray, J. W. (1976). Toppling of Rock Slopes. *Rock Engineering for Foundations and Slopes* (pp. 201 - 234). New York: American Society of Civil Engineers.

RocTopple was used to analyze a slope with geometry given in the article. The slope is subject to block toppling. The analysis comprised of computing the factor of safety in *RocTopple*, and then the geometry was exported to *RS2* to find an equivalent shear strength reduction factor. *RocTopple* results were also verified using rigid blocks in UDEC.

Geometry and Material Properties

Note that the geometry in *RocTopple* has been modified. As a result, the model has different block heights than those calculated in the original publication. The key difference is that block 1 now stands alone (height does not exceed step) with a total of 14 blocks, and the failure of the slope depends on the equilibrium of block 2. We also performed analyses with only 13 blocks to observe the differences although the first block was still separate from the rest of the blocks. The 13 blocks *RocTopple* model can be created by modifying the Joint Spacing to 10.4m.

| Analysis | φ΄ (deg.) | γ (kN/m³) |
|-----------|--------------|--------------|
| Example 2 | 21.455 | 25.0 |

Table 1.2.1: Material Properties

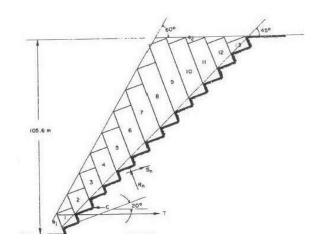


Figure 1.2.1: Goodman and Bray Example 2 Geometry (13 Blocks)

1.2.2. RocTopple Analysis

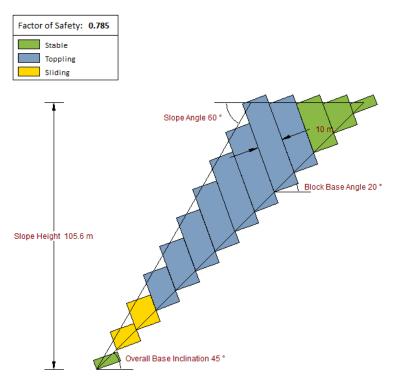


Figure 1.2.2: RocTopple Geometry (14 Blocks, Separate First Block)

1.2.3. Building a Compatible RS2 Model

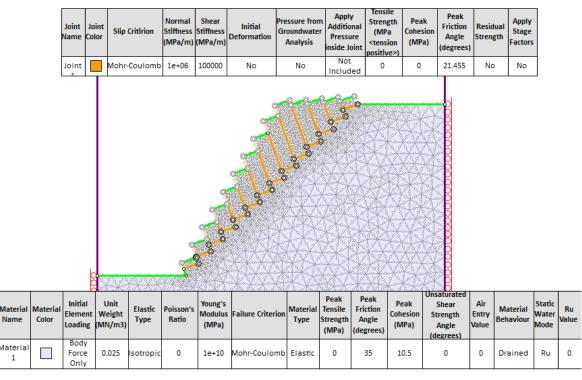


Figure 1.2.3: RS2 Geometry and Properties (14 Blocks)

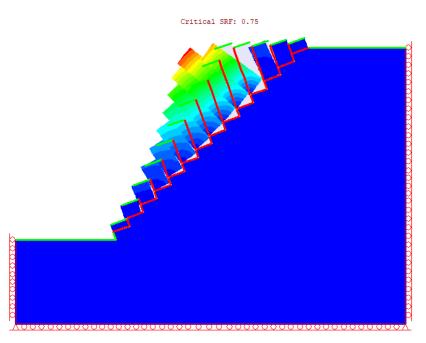
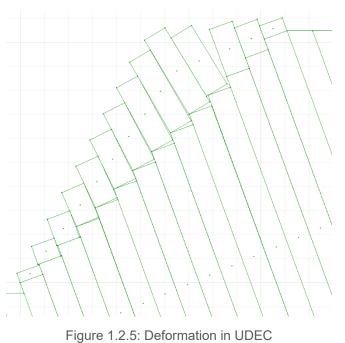


Figure 1.2.4: RS2 Total Displacement Contours and Deformed Shape

1.2.4. UDEC Analysis



1.2.5. Results

| | RocTopple | RS2 | UDEC | Goodman and Bray |
|-----------|-----------|------|------|---------------------|
| 14 Blocks | 0.79 | 0.75 | 0.69 | N/A |
| 13 Blocks | 0.99 | 0.74 | N/A | 1.0 |

Table 1.2.2: Factors of Safety

1.3. RocTopple Verification Problem #3

[RocTopple Build 2.001]

1.3.1. Problem Description

This verification looks at the block toppling example from:

Alejano, L. R., & Alonso, E. (2005). Application of the 'Shear and Tensile Strength Reduction Technique' to Obtain Factors of Safety of Toppling and Footwall Rock slopes. *Eurock: Impact of Human Activity on the Geological Environment*.

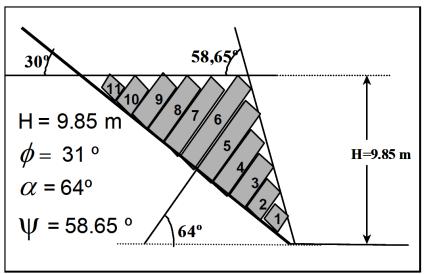
A block toppling model was constructed and analyzed in *RocTopple* using geometric data given in the article. The model was then exported to *RS2*, in which shear strength reduction analysis was used to verify factor of safety results. Results were also verified using rigid block UDEC analysis.

Note that the article does not specify a width for the blocks. Block width of 1.75m was used in the *RocTopple* model to achieve the eleven blocks as seen in the article.

Geometry and Material Properties

| Slope Height (m) | Slope Angle (deg) | Joint Angle (deg) | Overall Base Inclination (deg) | $oldsymbol{\phi}'$ (deg) | γ (kN/m³) |
|---------------------|----------------------|----------------------|--------------------------------------|--------------------------|--------------|
| 9.85 | 58.65 | 64 | 30 | 31 | 25.0 |

Table 1.3.1: Material Properties





1.3.2. RocTopple Analysis

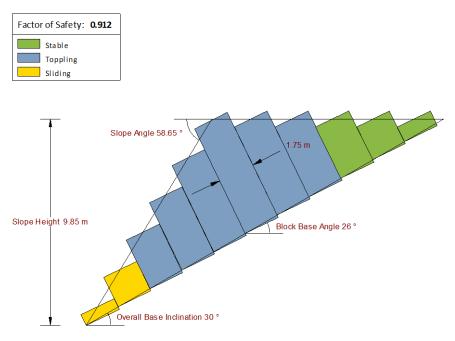


Figure 1.3.2: RocTopple Geometry

1.3.3. Building a Compatible RS2 Model

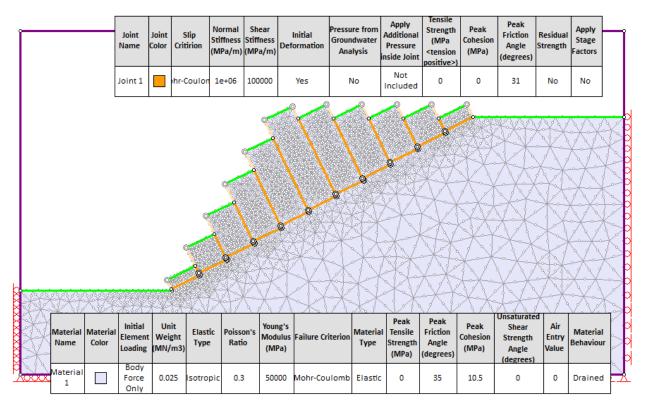


Figure 1.3.3: RS2 Geometry and Properties

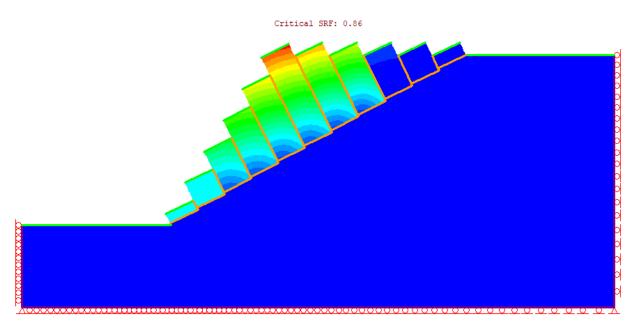


Figure 1.3.4: RS2 Displacement Contours

1.3.4. UDEC Analysis

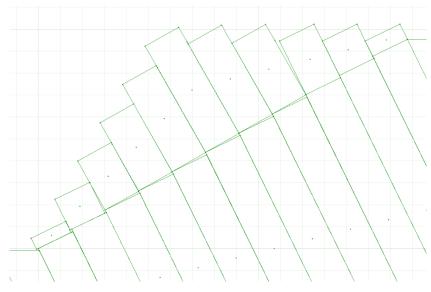


Figure 1.3.5: Deformation in UDEC

1.3.5. Results

Table 1.3.2: Factors of Safety

| RocTopple | RS2 | UDEC | Alejano and Alonso |
|-----------|------|------|-----------------------|
| 0.91 | 0.86 | 0.88 | 0.76 |

1.4. RocTopple Verification Problem #4

[RocTopple Build 2.001]

1.4.1. Problem Description

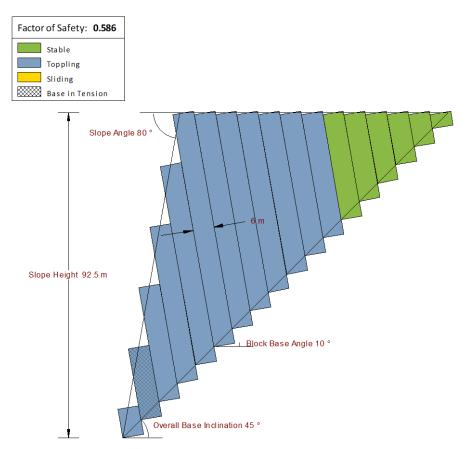
This verification problem examines the case of block toppling in a steep slope.

Geometry and Material Properties



| Material | Joints |
|------------------------------------|-----------------|
| Unit Weight = 2.5 t/m ³ | ϕ = 38.15° |

1.4.2. RocTopple Analysis





1.4.3. Building a Compatible RS2 Model

Results are verified in UDEC and *RS2*. Both programmes also predict that blocks are toppling from the 7th block from the top all the way to the toe block. These programs also generated comparable factors of safety.

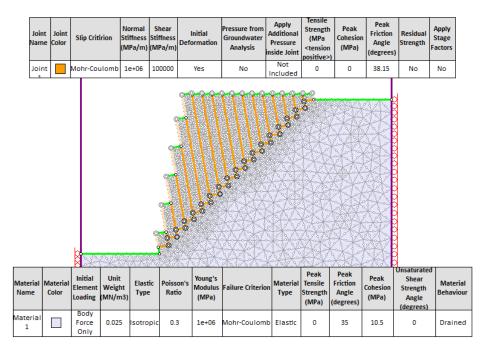


Figure 1.4.2: RS2 Geometry and Properties

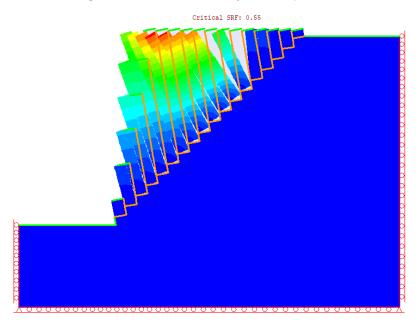


Figure 1.4.3: RS2 Displacement Contours

1.4.4. Results

Table 1.4.2: Factors of Safety

| RocTopple | RS2 | UDEC |
|-----------|------|------|
| 0.59 | 0.55 | 0.59 |

1.5. *RocTopple* Verification Problem #5

[RocTopple Build 2.001]

1.5.1. Problem Description

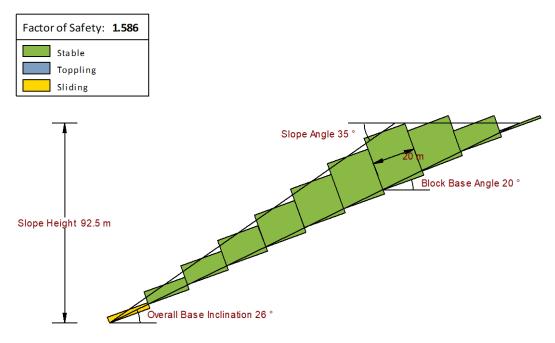
This verification problem examines the case of sliding blocks on a slope.

Geometry and Material Properties



| Material | Joints |
|------------------------------------|---------------------|
| Unit Weight = 2.5 t/m ³ | $\phi = 30^{\circ}$ |

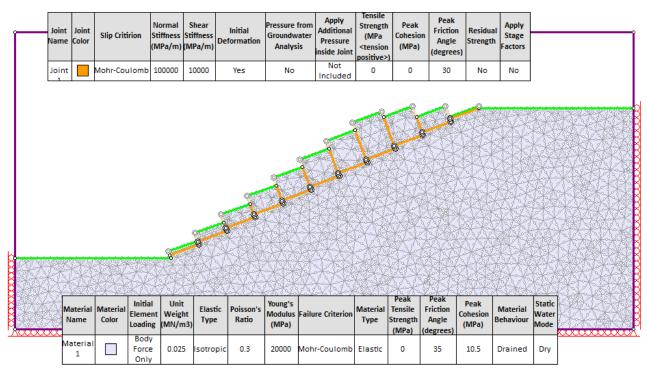
1.5.2. RocTopple Analysis





RocTopple predicts that blocks are sliding critical at the point of failure.

Results were verified in *RS2* and RocPlane, which uses the limit equilibrium method to predict the factor of safety for 2-D planar failure. The analysis in RocPlane used a failure plane angle of 20°.



1.5.3. Building a Compatible RS2 Model

Figure 1.5.2: RS2 Geometry and Properties

Critical SRF: 1.58

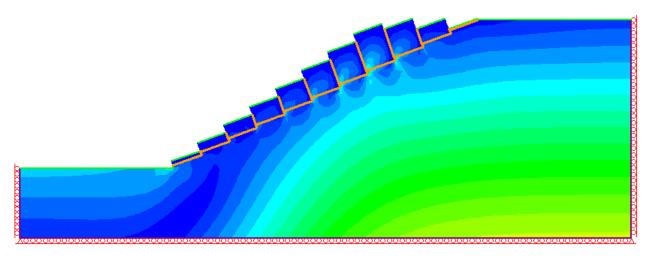


Figure 1.5.3: RS2 Displacement Contours

1.5.4. Results

| Table | 1.5.2: | Factors | of Safety |
|--------|--------|---------|-----------|
| I GDIO | 1.0.2. | 1 00010 | orourouy |

| RocTopple | RS2 | RocPlane |
|-----------|------|----------|
| 1.59 | 1.58 | 1.59 |

1.6. *RocTopple* Verification Problem #6

[RocTopple Build 2.001]

1.6.1. Problem Description

This verification problem examines the Barton-Bandis Joint Shear Strength model.

Geometry and Material Properties

| | Material | | Joints | |
|---|------------------------------------|-----|------------|------|
| | | JRC | JCS (t/m²) | PhiR |
| Α | | 10 | 10000 | 30° |
| В | Unit Weight = 2.5 t/m ³ | 8 | 7000 | 20° |
| С | | 5 | 5000 | 15° |

Table 1.6.1: Properties

1.6.2. RocTopple Analysis

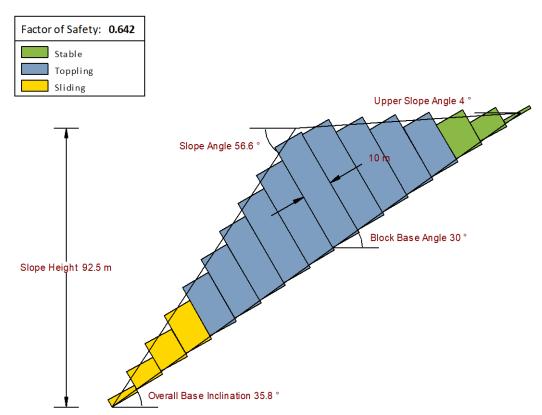
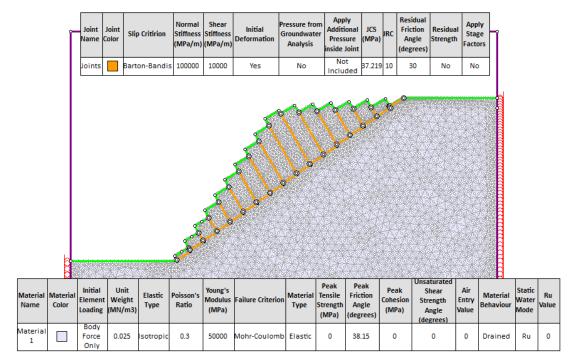


Figure 1.6.1: RocTopple Geometry of Example 6c and Block Failure Modes at Limit Equilibrium

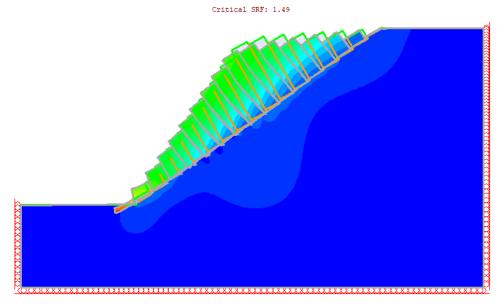
Results were verified using manual shear strength reduction in *RS2*. The joint strength parameters could not be divided by the factor of safety values in finding a shear strength reduction factor because the Barton Bandis model is non-linear. Instead, normal and shear stress data at the given shear strength model had to be exported to Excel from RocData, where the shear stresses were manually adjusted for

different factors of safety (shear stress/FS). The normal stress and new shear stress values were imported back into RocData, which uses the Levenberg-Marquardt algorithm to fit the stress values to a set of Barton Bandis parameters. Finally, the slope stability was evaluated using stress analysis in *RS2* given the adjusted parameters. A discrepancy is seen in one of the factors of safety because the parameters did not give a perfect fit to the stress data. As seen in Table 6-2, factors of safety between *RocTopple* and *RS2* do not agree when there are large residuals in the parameter fitting process.



1.6.3. Building a Compatible RS2 Model

Figure 1.6.2: RS2 Geometry and Properties for Example 6a





1.6.4. Results

| | Factors of Safety | | RocData Residuals | |
|---|-------------------|------|------------------------|--|
| | RocTopple | RS2 | (Fit at <i>RS2</i> FS) | |
| A | 1.93 | 1.49 | 17.964 | |
| В | 1.07 | 0.96 | 0.020 | |
| С | 0.64 | 0.57 | 4.414 | |

Table 1.6.2: Factors of Safety

1.7. RocTopple Verification Problem #7

[RocTopple Build 2.001]

1.7.1. Problem Description

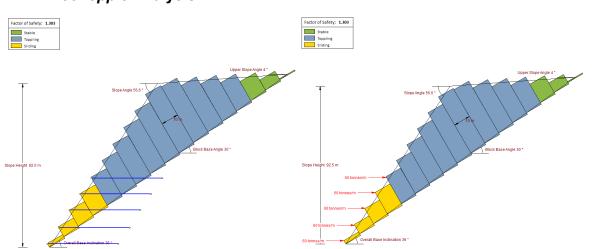
This verification problem examines the application of bolts and line loads.

Since the formulation for end-anchored bolts consists of having two forces applied at the two ends, having a bolt that is anchored in the slope bedrock is equivalent to having a line load applied at where the bolt is installed (Table 1.7.1).

Geometry and Properties







1.7.2. *RocTopple* Analysis

Figure 1.7.1: *RocTopple* Geometry with Bolts Each at 60 tonnes/m (left); Equivalent Line Loads at 60 tonnes/m (right)

1.7.3. Building a Compatible RS2 Model

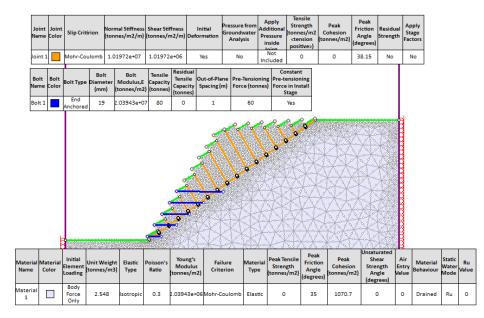


Figure 1.7.2: RS2 Geometry and Properties for Bolts

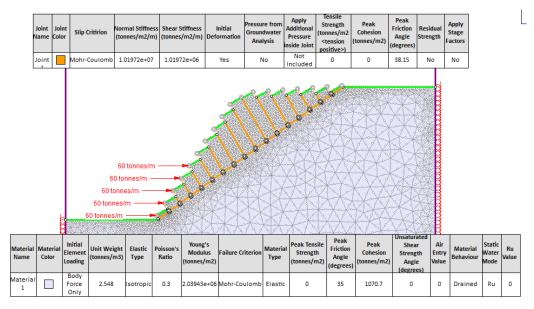


Figure 1.7.3: RS2 Geometry and Properties for Equivalent Line Loads

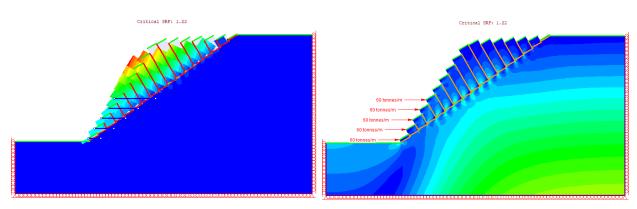


Figure 1.7.4: RS2 Displacement Contours for Bolts (left) and Equivalent Line Loads (right)

1.7.4. Results

| Table | 1.7.2: | Factors | of Safety |
|-------|--------|---------|-----------|
|-------|--------|---------|-----------|

| Example | RocTopple | RS2 |
|--------------------|-----------|------|
| 7A with Bolts | 1.30 | 1.22 |
| 7B with Line Loads | 1.30 | 1.22 |

1.8. RocTopple Verification Problem #8

[RocTopple Build 2.001]

1.8.1. Problem Description

This verification problem examines the application of distributed loads.

Geometry and Properties



| Material | Joints |
|------------------------------------|-----------------|
| Unit Weight = 2.5 t/m ³ | ϕ = 38.15° |

1.8.2. RocTopple Analysis

Case 1:

Distributed loads are assumed to apply on top of blocks and are taken into account in the calculation as equivalent line loads.

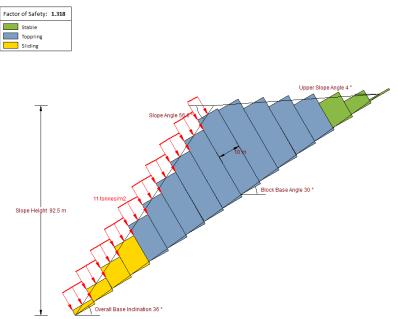
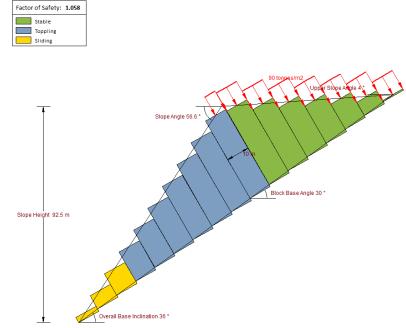


Figure 1.8.1: *RocTopple* Slope Face Pressure of 11 tonnes/m²

Case 2:



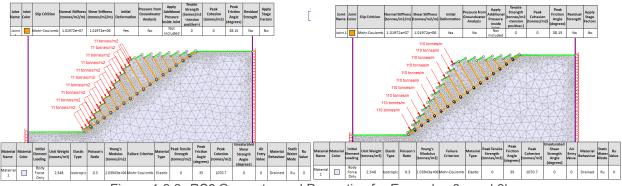
A similar analysis for pressure on the upper slope face is illustrated below.



The example was verified in two ways. The first was by applying equivalent line loads in *RocTopple*, and the second was to model the slope in *RS2* using distributed loads and by equivalent line loads.

1.8.3. Building a Compatible *RS2* Model

Case 1:





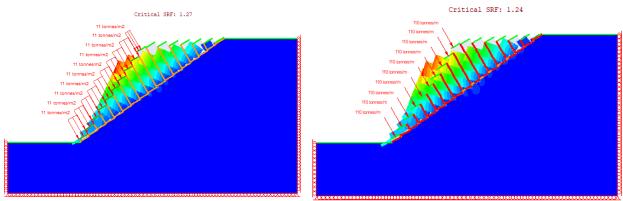


Figure 1.8.4: RS2 Displacement Contours for Examples 8a and 8b

Case 2:

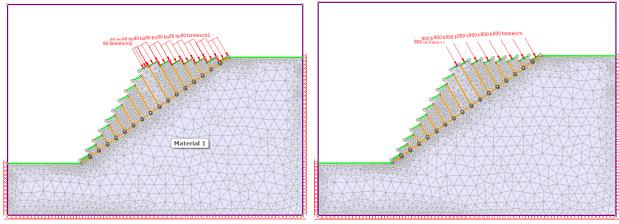


Figure 1.8.5: RS2 Geometry for Examples 8c and 8d

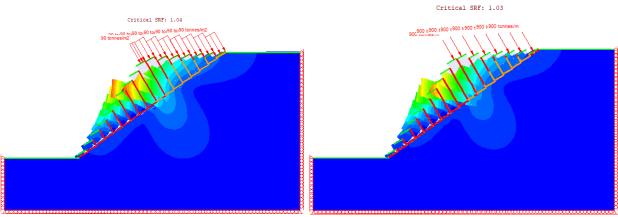


Figure 1.8.6: RS2 Displacement Contours for Examples 8c and 8d

1.8.4. Results

| Example | Note | RocTopple | RS2 |
|---------|--|-----------|------|
| 8A | Distributed Load (11 tonnes/m ²) | 1.32 | 1.27 |
| 8B | Equivalent Line Loads | 1.32 | 1.24 |

Table 1.8.2: Factors of Safety for Model with Slope Face Pressure

Table 1.8.3: Factors of Safety for Model with Upper Slope Face Pressure

| Example | Notes | RocTopple | RS2 |
|---------|--|-----------|------|
| 8C | Distributed Load (90 tonnes/m ²) | 1.06 | 1.04 |
| 8D | Equivalent Line Loads | 1.07 | 1.03 |

1.9. *RocTopple* Verification Problem #9

[RocTopple Build 2.001]

1.9.1. Problem Description

This verification problem examines the Mohr-Coulomb Joint Shear Strength model.

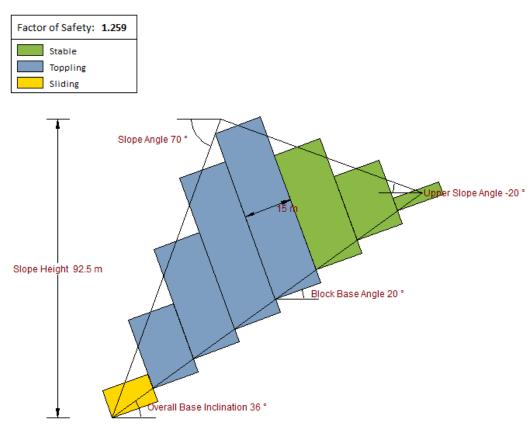
Geometry and Properties

| | | J | oints |
|---------|------------------------------------|----------|-------------------------|
| Example | Material | φ (°) | Cohesion (tonnes/m²) |
| A | | 38.15 | 0 |
| В | | 30 | 10 |
| С | Unit Weight = 2.5 t/m ³ | 25 | 25 |
| D | | 10 | 40 |
| E | | 0 | 50 |

Table 1.9.1: Properties

1.9.2. RocTopple Analysis

Results for a series of analyses using Mohr-Coulomb shear strength are shown below. The analyses represent a variety of combinations of friction angle and cohesion.





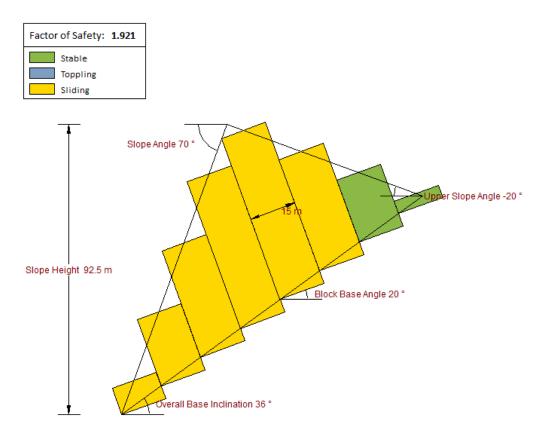
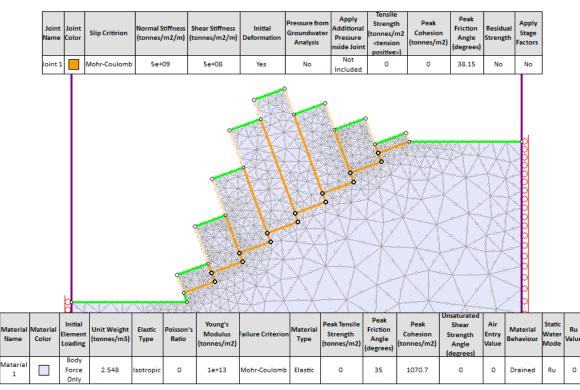
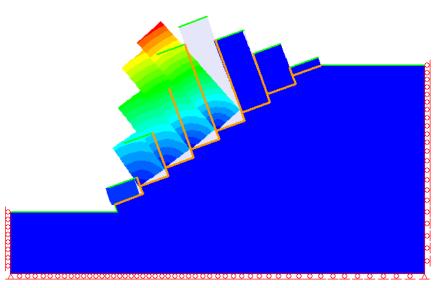


Figure 1.9.2: *RocTopple* Failure Mode of Blocks of Slopes B, C, D and E (Screen Capture for Model B)



1.9.3. Building a Compatible RS2 Model

Figure 1.9.3: RS2 Geometry and Properties for Example 9a



Critical SRF: 1.13

Figure 1.9.4: *RS2* Deformation and Yielded Joints for Example 9a (Same Failure Mode as Examples 9b and 9c)

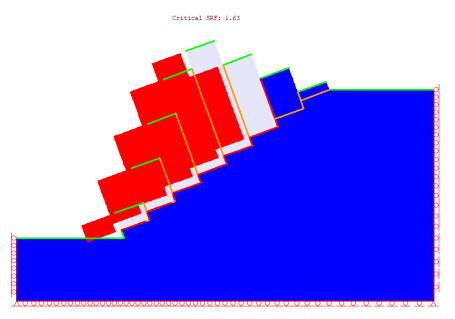


Figure 1.9.5: RS2 Deformation and Yielded Joints for Example 9e (Same Failure Mode as Example 9d)

1.9.4. Results

| Table | 1.9.2: | Factor | of | Safety |
|-------|--------|--------|----|--------|
|-------|--------|--------|----|--------|

| | φ (°) | Cohesion (tonnes/m²) | RocTopple | RS2 |
|---|-------|----------------------|-----------|------|
| A | 38.15 | 0 | 1.26 | 1.13 |
| В | 30 | 10 | 1.92 | 1.97 |
| С | 25 | 25 | 2.12 | 2.15 |
| D | 10 | 40 | 1.82 | 1.81 |
| E | 0 | 50 | 1.67 | 1.63 |

1.10. *RocTopple* Verification Problem #10

[RocTopple Build 2.001]

1.10.1. Problem Description

This verification problem examines the application of seismic loads.

A shallow slope with all sliding critical blocks at the point of failure, is now exhibiting toppling failure under a large seismic load.

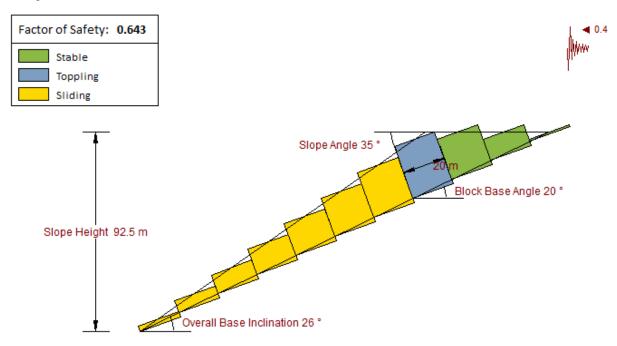
Geometry and Properties



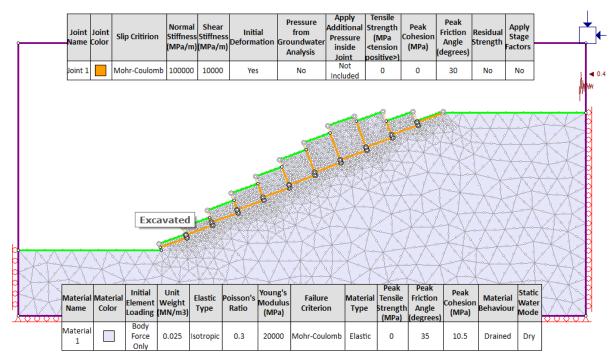
| Material | Joints |
|------------------------------------|---------------------|
| Unit Weight = 2.5 t/m ³ | $\phi = 30^{\circ}$ |

1.10.2. RocTopple Analysis

The same slope from Verification Example #5 now exhibits toppling behavior under a horizontal seismic loading coefficient of 0.4







1.10.3. Building a Compatible RS2 Model

Figure 1.10.2: RS2 Geometry and Properties

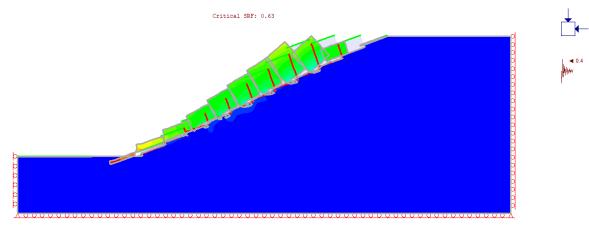


Figure 1.10.3: RS2 Deformation and Yielded Joints

1.10.4. Results

Table 1.10.2: Factors of Safety

| RocTopple | RS2 |
|-----------|------|
| 0.64 | 0.63 |

1.11. *RocTopple* Verification Problem #11

[RocTopple Build 2.001]

1.11.1. Problem Description

This verification problem examines the application of water pressure.

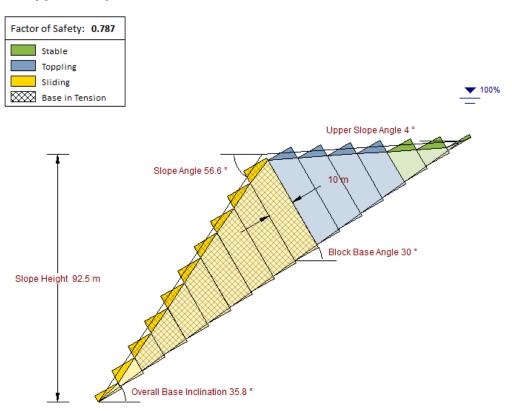
A slope with 100% fill joints in *RocTopple* is modelled in *RS2* using a phreatic surface that fully spans across the joints. The pressure is calculated using the Hu Auto option, which extrapolates the phreatic surface at a 45° angle. This example is modified from the slope in Verification Example #1.

Geometry and Properties



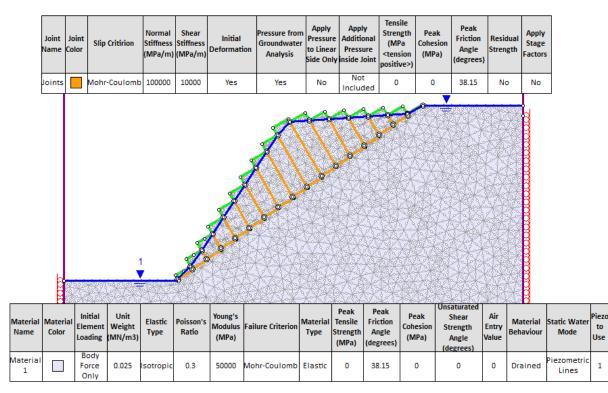
| Material | Joints |
|------------------------------------|------------------------|
| Unit Weight = 2.5 t/m ³ | $\phi = 38.15^{\circ}$ |

1.11.2.*RocTopple* Analysis





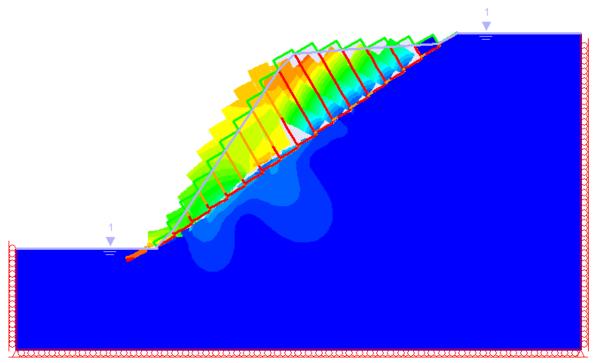
The model shows sliding blocks starting from the crest block to the toe.



1.11.3. Building a Compatible RS2 Model

Figure 1.11.2: RS2 Geometry and Properties

Critical SRF: 0.71





1.11.4. Results

| RocTopple | RS2 |
|-----------|------|
| 0.79 | 0.71 |

Note that while *RocTopple* reports tension at base of sliding blocks, *RS2* does not. Also note that while *RocTopple* assumes all joints are fully mobilized in shear, *RS2* results reflect that not all joints (i.e. toppling joints) are fully yielded for the sliding blocks (Figure 1.11.3). When shear is fully mobilized in the toppling joints, as is the case in *RocTopple*, it creates an uplifting force on the blocks and in the calculation results in base tension.

1.12. *RocTopple* Verification Problem #12

[RocTopple Build 2.001]

1.12.1. Problem Description

This verification problem examines the case of upslope toppling blocks.

When there are external forces, blocks may topple upslope. *RocTopple* provides warning when the slope may be toppling up. Note that *RocTopple* only checks for upslope stability for group blocks (blocks that are in contact with other blocks), and for only the toppling failure mode (rotation about the upper base corner).

Geometry and Properties

| Table | 1.12. | 1: | Properties |
|-------|-------|----|------------|
|-------|-------|----|------------|

| Material | Joints |
|------------------------------------|---------------------|
| Unit Weight = 2.5 t/m ³ | $\phi = 40^{\circ}$ |



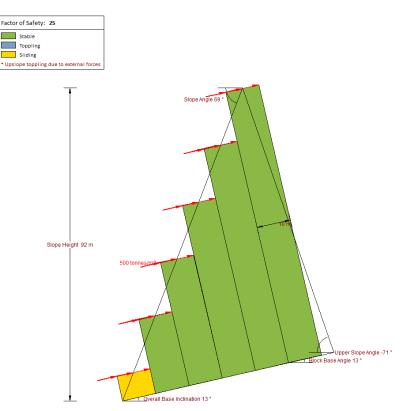


Figure 1.12.1: RocTopple Geometry with a Pressure of 500t/m² Supporting the Slope

The slope is stable in terms of downslope failure (factor of safety exceeding 25), but is unstable in terms of toppling upslope.

1.12.3. Building a Compatible RS2 Model

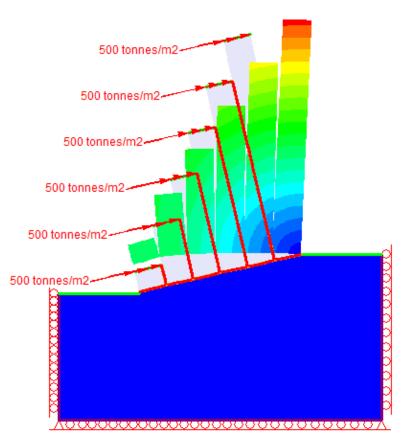


Figure 1.12.2: RS2 Stress Analysis

RS2 stress analysis confirms that the blocks are rotating upslope.

2. *RocTopple* Block-Flexural Toppling Verification

Analyses of block-flexure toppling were performed in *RocTopple* and verified with Finite Element Analysis using *RS2*. FS obtained from *RocTopple* was compared to the SRF obtained in *RS2*.

2.1. RocTopple Verification Problem #1

[RocTopple Build 2.001]

2.1.1. Problem Description

This verification problem examines a linear plane geometry.

Geometry and Material Properties

With the given geometry below:

| Table 2.1.1: Geometry |
|-----------------------|
|-----------------------|

| Parameter | Value |
|---|-------|
| Face Slope Angle (°) | 57 |
| Height (m) | 93 |
| Block/Column Thickness (m) | 10 |
| Overall Base Inclination Angle (°) | 30 |
| Upper Slope Angle (°) | 0 |
| Point of Application (Sliding/Shearing Block Above) Ratio | 0.75 |
| Point of Application (Bending Block Above) Ratio | 0.9 |

Examples 1a, 1b, 1c and 1d were investigated and are listed below.

| Table | 2.1.2: | Material | Properties |
|-------|--------|----------|------------|
|-------|--------|----------|------------|

| | Angle of Friction of Joints (°) | Cohesion of Joint (kPa) | Tensile Strength of Joints (kPa) | Angle of Friction of Rock (°) | Cohesion of Rock (kPa) | Tensile Strength of Rock (kPa) | Density (kN) |
|------------|--|-------------------------------|---|--|------------------------------|---|-----------------|
| Example 1a | 38 | 100 | 100 | 50 | 1000 | 50 | 27 |
| Example 1b | 26 | 50 | 50 | 40 | 1000 | 100 | 27 |
| Example 1c | 45 | 200 | 100 | 60 | 4000 | 100 | 32 |
| Example 1d | 44 | 160 | 46 | 56 | 2540 | 82 | 19 |

2.1.2. RocTopple Analysis

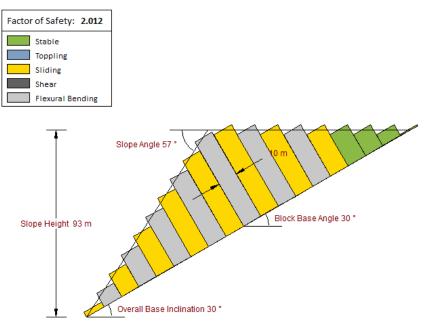


Figure 2.1.1: RocTopple Model of Example 1a

RocTopple does not account for solids deforming in the toppling process. Therefore, when conducting *RS2* Analysis, the stiffness of the rock was assumed to be high, with a Young's Modulus of 2000 GPa, and a poisons ratio of 0.1.

2.1.3. Building a Compatible RS2 Model

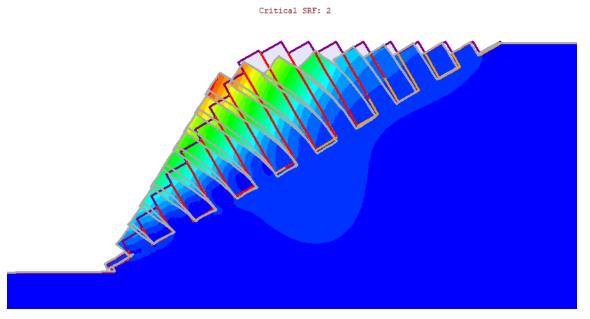


Figure 2.1.2: RS2 Total Displacement Contours of Example 1a at Critical SRF

2.1.4. Results

| Table 2.1.3: | Factors | of Safety |
|--------------|---------|-----------|
|--------------|---------|-----------|

| | SRF (<i>RS2</i>) | FS (<i>RocToppl</i> e) Final |
|------------|--------------------|----------------------------------|
| Example 1a | 2.0 | 2.01 |
| Example 1b | 1.25 | 1.27 |
| Example 1c | 2.85 | 2.78 |
| Example 1d | 3.05 | 3.04 |

2.2. RocTopple Verification Problem #2

[RocTopple Build 2.001]

2.2.1. Problem Description

This verification problem examines another linear plane geometry.

Geometry and Material Properties

With the given geometry below:

| Parameter | Value |
|---|-------|
| Face Slope Angle (°) | 78 |
| Height (m) | 85 |
| Block/Column Thickness (m) | 7.6 |
| Upper Slope Angle (°) | 0 |
| Dip Angle | 39 |
| Overall Base Inclination Angle (°) | 51 |
| Point of Application (Sliding/Shearing Block Above) Ratio | 0.59 |
| Point of Application (Bending Block Above) Ratio | 0.9 |

4 examples (with varying material properties) were investigated and the results are listed below.

| | Angle of Friction of Joints (°) | Cohesion of Joint (kPa) | Tensile Strength of Joints (kPa) | Angle of Friction of Rock (°) | Cohesion of Rock (kPa) | Tensile Strength of Rock (kPa) | Density (kN) |
|-------------|--|-------------------------------|---|--|------------------------------|---|-----------------|
| Example 2a | 38 | 100 | 100 | 40 | 1000 | 100 | 27 |
| Example 2b | 25 | 50 | 50 | 54 | 1200 | 85 | 27 |
| Example 2c | 45 | 250 | 150 | 60 | 4000 | 100 | 33 |
| Example 2d | 30 | 60 | 40 | 43 | 800 | 52 | 23 |
| Example 2d2 | Base: 30 Bed: 50 | Base: 60 Bed: 100 | Base: 40 Bed: 100 | 43 | 800 | 52 | 23 |

Table 2.2.2: Material Properties

Geotechnical tools, inspired by you.

2.2.2. RocTopple Analysis

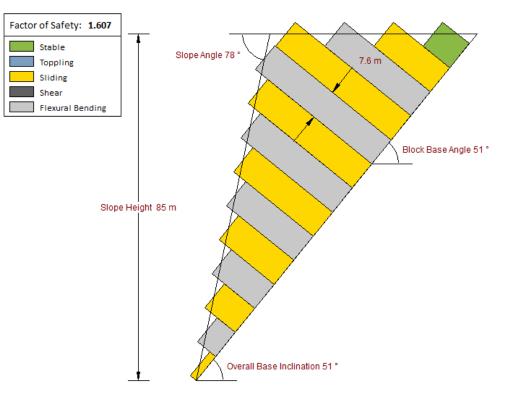
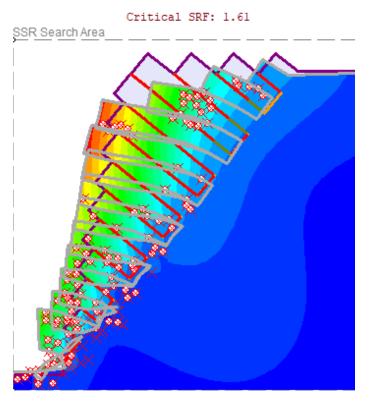


Figure 2.2.1: RocTopple Model of Example 2a

2.2.3. Building a Compatible RS2 Model





2.2.4. Results

| | SRF (<i>RS2</i>) | FS (<i>RocTopple</i>) Final |
|-------------|--------------------|----------------------------------|
| Example 2a | 1.61 | 1.61 |
| Example 2b | 1.01 | 0.96 |
| Example 2c | 2.34 | 2.27 |
| Example 2d | 1.22 | 1.16 |
| Example 2d2 | 1.89 | 1.76 |

| Table | 222. | Factors | of | Safety |
|-------|--------|---------|----|--------|
| rapie | Z.Z.J. | raciors | 0I | Salety |

2.3. RocTopple Verification Problem #3

[RocTopple Build 2.001]

2.3.1. Problem Description

This verification problem examines the case where shear failure occurs.

Geometry and Material Properties

With the given geometry below:

| Parameter | Value |
|---|-------|
| Face Slope Angle (°) | 41 |
| Height (m) | 93 |
| Block/Column Thickness (m) | 13 |
| Upper Slope Angle (°) | 0 |
| Dip Angle | 60 |
| Overall Base Inclination Angle (°) | 30 |
| Point of Application (Sliding/Shearing Block Above) Ratio | 0.75 |
| Point of Application (Bending Block Above) Ratio | 0.9 |

3 examples with varying material properties were investigated and the results are shown below.

Table 2.3.2: Material Properties

| | Angle of Friction of Joints (°) | Cohesion of Joint (kPa) | Tensile Strength of Joints (kPa) | Angle of Friction of Rock (°) | Cohesion of Rock (kPa) | Tensile Strength of Rock (kPa) | Density (kN) |
|------------|--|-------------------------------|---|--|------------------------------|---|-----------------|
| Example 3a | 30 | 50 | 50 | 34 | 400 | 50 | 40 |
| Example 3b | 25 | 45 | 40 | 30 | 300 | 60 | 40 |
| Example 3c | 36 | 85 | 80 | 60 | 600 | 130 | 35 |

2.3.2. RocTopple Analysis

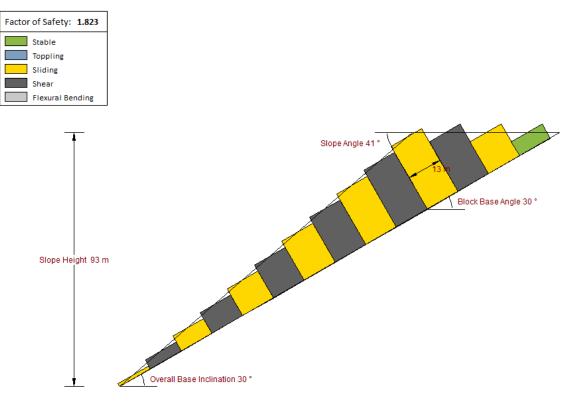


Figure 2.3.1: RocTopple Model of Example 3a

2.3.3. Building a Compatible RS2 Model

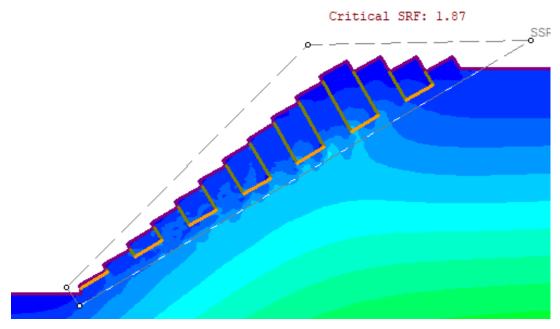


Figure 2.3.2: RS2 Results of Example 3a at Critical SRF

2.3.4. Results

| | FS (<i>RocToppl</i> e) Final | SRF (<i>RS2</i>) |
|------------|-------------------------------------|-----------------------|
| Example 3a | 1.82 | 1.87 |
| Example 3b | 1.47 | 1.50 |
| Example 3c | 3.45 | 3.60 |

Table 2.3.3: Factors of Safety

2.4. RocTopple Verification Problem #4

[RocTopple Build 2.001]

2.4.1. Problem Description

This verification problem examines the Barton-Bandis Joint Shear Strength model.

Geometry and Material Properties

The geometry identical to Verification Example #1.

3 examples with varying Barton-Bandis (BB) Shear Strength models were investigated.

| | JRC | JCS (kPa) | PhiR | Angle of Friction of Rock (°) | Cohesion of Rock (kPa) | Tensile Strength of Rock (kPa) | Density (kN) |
|------------|-----|-----------|------|-------------------------------------|------------------------------|--------------------------------------|-----------------|
| Example 4a | 10 | 10000 | 30° | | | | 32 |
| Example 4b | 8 | 7000 | 20° | 45 | 800 | 50 | 19 |
| Example 4c | 5 | 500 | 15° | | | | 32 |

Table 2.4.1: Material Properties

Examples with equivalent Mohr-Coulomb (MC) setup were also investigated for comparison.

 Table 2.4.2: Mohr-Coulomb Shear Strength Properties

| | Cohesion (kPa) | Friction Angle (°) |
|------------|----------------|-----------------------|
| Example 4a | 79.5 | 36.6 |
| Example 4b | 39.5 | 24.7 |
| Example 4c | 17.2 | 12.6 |

2.4.2. *RocTopple* Analysis

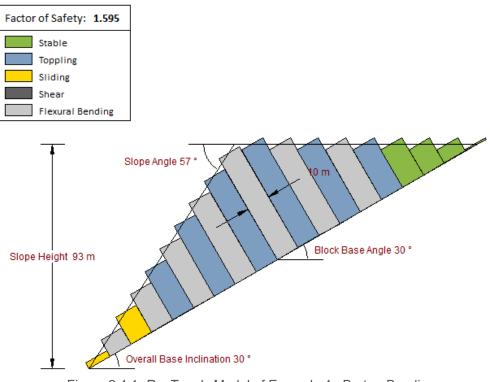


Figure 2.4.1: RocTopple Model of Example 4a Barton-Bandis

2.4.3. Building a Compatible RS2 Model

Critical SRF: 1.75

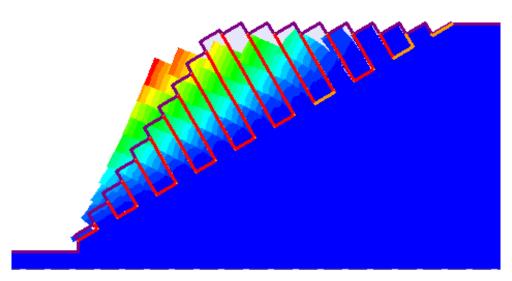


Figure 2.4.2: RS2 Results of Example 4a

2.4.4. Results

| Table | 2.4.3: | Factors | of | Safety |
|-------|--------|---------|----|--------|
|-------|--------|---------|----|--------|

| | SRF (<i>RS2</i>) | FS (<i>RocTopple</i>) MC | FS (<i>RocTopple</i>) BB |
|------------|--------------------|----------------------------------|----------------------------------|
| Example 4a | 1.75 | 1.67 | 1.60 |
| Example 4b | 1.25 | 1.21 | 1.10 |
| Example 4c | 0.55 | 0.51 | 0.52 |

2.5. RocTopple Verification Problem #5

[RocTopple Build 2.001]

2.5.1. Problem Description

This verification problem examines the application of bolts and line loads.

Geometry and Material Properties

The geometry and strength properties are given in Example 1a and 1b, Example 5a and 5b; bolts and line loads are installed, respectively.

2.5.2. RocTopple Analysis

Bolts Model

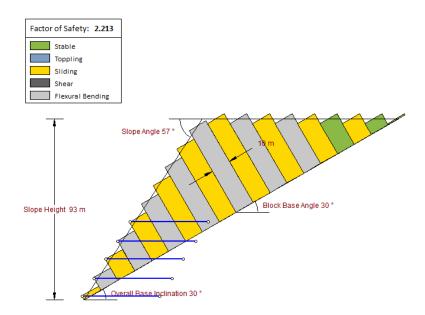


Figure 2.5.1: *RocTopple* Model of Example 5a, Bolt Capacity = 600 kN

Line Loads Model

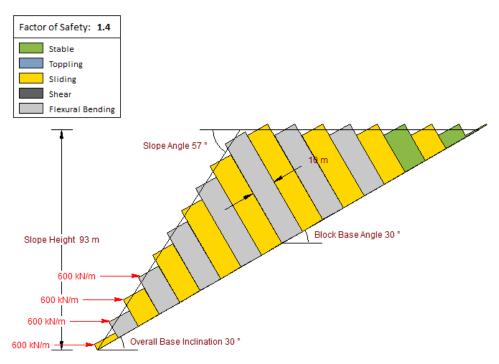
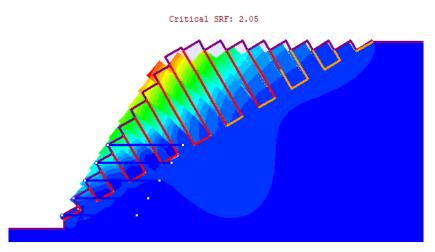


Figure 2.5.2: RocTopple Model of Example 5b, Line Loads = 600 kN

2.5.3. Building a Compatible RS2 Model

Bolts Model





Line Loads Model

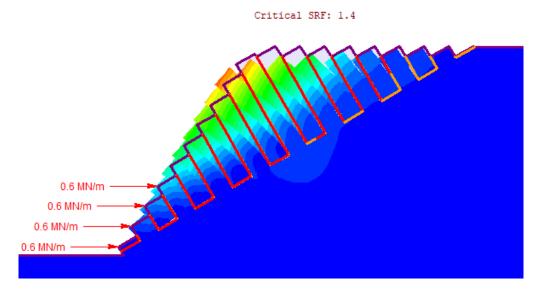


Figure 2.5.4: RS2 Results of Example 5b, Line Loads = 600 kN

2.5.4. Results

Results are shown below.

| | FS (<i>RocTopple</i>) Final | SRF (<i>RS2</i>) |
|------------|-------------------------------------|--------------------|
| Example 5a | 2.21 | 2.05 |
| Example 5b | 1.40 | 1.40 |

Table 2.5.1: Factors of Safety

2.6. RocTopple Verification Problem #6

[RocTopple Build 2.001]

2.6.1. Problem Description

This verification problem examines the application of distributed loads.

Geometry and Material Properties

The geometry and strength properties identical to Example 3b.

Forces

Example 6 is analyzed with distributed load applied.



| | Distributed Load |
|-----------|------------------|
| Example 6 | 300 kN |

2.6.2. RocTopple Analysis

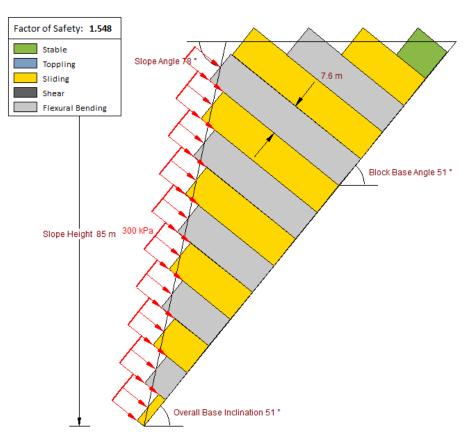


Figure 2.6.1: RocTopple Model of Example 6

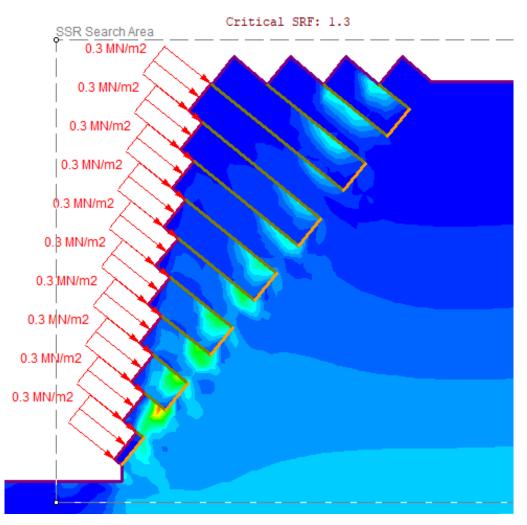


Figure 2.6.2: RS2 Results of Example 6

2.6.3. Results

| | FS (<i>RocTopple</i>) Final | SRF (<i>RS2</i>) |
|-----------|----------------------------------|--------------------|
| Example 6 | 1.55 | 1.30 |

2.7. RocTopple Verification Problem #7

[RocTopple Build 2.001]

2.7.1. Problem Description

This verification problem examines the application of seismic loads.

Geometry and Material Properties

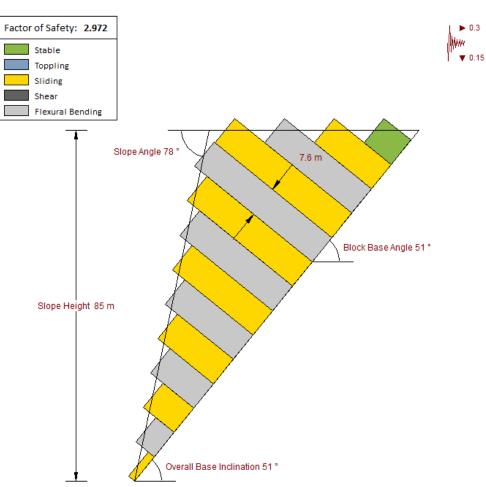
With the geometry and strength properties given in Example 3c, apply the following for Example 7.

Forces

Table 2.7.1: Seismic Coefficient

| | Seismic Coefficient | |
|-----------|--------------------------------|--|
| Example 7 | Horizontal: 0.3 (to the right) | |
| | Vertical: 0.15 (down) | |

2.7.2. RocTopple Analysis





2.7.3. Building a Compatible RS2 Model

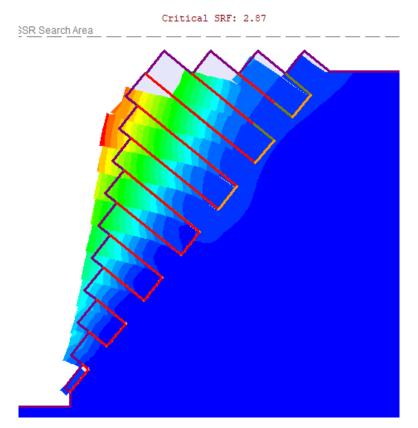


Figure 2.7.2: RS2 Result of Example 7

2.7.4. Results

| | FS (<i>RocToppl</i> e) Final | SRF (<i>RS2</i>) |
|-----------|----------------------------------|--------------------|
| Example 7 | 2.97 | 2.87 |